

# A UNIFIED APPROACH TO FIRE SPREAD MODELLING

A parable of model parsimony

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## OUTLINE OF TALK

- Modelling the spread of fire
- Model parsimony
- Review of current models for fire rate of spread
- A simple index for fire spread
- Model comparisons
- Implications and conclusions

## **MODELLING THE SPREAD OF FIRE**

One of the main goals of wildfire research is to provide a relatively simple and timely answer to the question:

**“What is the fire’s forward rate of spread”**

A number of answers to this question have been provided depending on vegetation type and the availability of empirical fire spread data.

## MODELLING THE SPREAD OF FIRE

Fire spread models typically take the form of a mathematical function, or a series of functions, that take environmental data as inputs and deliver an expected rate of spread as an output.

The modelling procedure assumes a parametric functional form for the model, and then appeals to empirical data to estimate the model parameters.

$$R = aU^b \exp(-cm)$$

Model parameters  $a$ ,  $b$  and  $c$ .



$$R = 6.4211U^{0.9102} \exp(-0.0761m)$$

## MODEL PARSIMONY

### Occam's Razor or the Law of Parsimony...

A model should be as simple as possible and as complicated as necessary...!



# **REVIEW OF FIRE SPREAD MODELS**

## CSIRO GRASSLAND FIRE SPREAD MODEL

(Cheney et al. 1998)

- Rate of spread

$$R = \begin{cases} (0.054 + 0.269U)wMwC, & U < 5 \text{ km/h} \\ (1.4 + 0.838(U - 5)^{0.844})wMwC, & U \geq 5 \text{ km/h} \end{cases}$$

- Fuel moisture factor

$$wM = \begin{cases} \exp(-0.108m), & m < 12\% \\ 0.684 - 0.0342m, & m \geq 12\% \quad U < 10 \text{ km/h} \\ 0.547 - 0.0228m, & m \geq 12\% \quad U \geq 10 \text{ km/h} \end{cases}$$

- Fuel availability factor

$$wC = \frac{1.036}{1 + 103.99 \exp(-0.0996(C - 20))}$$

- Fuel moisture content

$$m = 9.58 - 0.205T + 0.138H$$

13+ parameter model...!

# **BUTTONGRASS MOORLANDS FIRE SPREAD MODEL**

(Marsden-Smedley and Catchpole 1995)

- Rate of spread     $R = 0.678(0.67U)^{1.312} \exp(-0.0243n)(1 - \exp(-0.116AGE))$

- Fuel moisture content       $m = \exp(1.660 + 0.0214H - 0.0292T_{dew})$

- Dewpoint temperature conversion (Lawrence, 2005 – BAMS)

$$T_{dew} = (T + 273.15) \left[ 1 - \frac{(T + 273.15) \ln\left(\frac{H}{100}\right)}{L / R_w} \right]^{-1} - 273.15$$

$L = 2.44 \times 10^6 \text{ J/kg at } 25^\circ\text{C}$   
 $R_w = 461.5 \text{ J/(K kg)}$

## 7+ parameter model...!

## S.A. HEATH FIRE SPREAD MODEL

(Cruz et al. 2010)

- Rate of spread

$$R = \begin{cases} 0, & P_S < 0.5 \\ 2.455(0.43U)^{1.2} \exp(-0.11m) FHS_{el}^{0.9}, & P_S \geq 0.5 \end{cases}$$

- Fuel moisture content

$$m = 4.79 + 0.173H - 0.1(T - 25) - \Delta 0.027H \quad \Delta = \begin{cases} 1, & 12:00 - 17:00 \text{ hrs, Oct-Mar} \\ 0, & \text{otherwise} \end{cases}$$

- Probability of successful fire spread (go/no-go)

$$P_s = \frac{1}{1 + \exp[-(2.926 + 2.132(0.43U) - 2.32m + 5.31PCS_{ns})]}$$

**6+ parameter model...!**

## TEMPERATE SHRUBLAND FIRE SPREAD MODEL

(Anderson et al. 2015)

- Rate of spread     $R = \begin{cases} [R_0 + 0.2(3.005 - R_0)U]h^{0.22} \exp(-0.076m), & U < 5 \text{ km/h} \\ 5.67(0.67U)^{0.91}h^{0.22} \exp(-0.076m), & U \geq 5 \text{ km/h} \end{cases}$
  - Fuel moisture content
- $$m = 4.37 + 0.161H - 0.1(T - 25) - \Delta 0.027H, \quad \Delta = \begin{cases} 1, & 12:00 - 17:00 \text{ hrs, Oct-Mar} \\ 0, & \text{otherwise} \end{cases}$$

10+ parameter model...!

## DRY EUCALYPT FOREST FIRE MODEL

(Cheney et al. 2012)

- Rate of spread

$$R = \begin{cases} 30\Phi M_f, & U \leq 5 \text{ km/h} \\ [30 + 1.531\Phi F(U - 5)^{0.858}] \Phi M_f, & U > 5 \text{ km/h} \end{cases}$$

- Fuel moisture factor

$$\Phi M_f = 18.35m^{-1.495}$$

- Fuel moisture content

$$m = \begin{cases} 2.76 - 0.0187T + 0.124H, & 12:00 - 17:00 \text{ hrs, Oct-Mar} \\ 3.60 - 0.0450T + 0.169H, & \text{Other daylight hours} \\ 3.08 - 0.0483T + 0.198H, & \text{Night-time hours} \end{cases}$$

- Fuel structure factor

$$\Phi F = 1.03FHS_s^{0.93}(FHS_{ns}h_{ns})^{0.637}$$

13+ parameter model...!

## SUMMARY OF CURRENT FIRE SPREAD MODEL PARSIMONY

| Vegetation type      | Number of model parameters* |
|----------------------|-----------------------------|
| Grasslands           | 13                          |
| Buttongrass moorland | 7                           |
| Mallee-Heath         | 6                           |
| Temperate shrubland  | 10                          |
| Dry eucalypt forest  | 13                          |

\* Only considering 'non-fuel' components.

However, from an intuitive point of view, in a particular fuel type/structure a fire should spread faster:

1. ***The stronger the wind***, and
2. ***The drier the fuel...***

***This is only 2 degrees of freedom...!?***

## A SIMPLE INDEX FOR FIRE SPREAD

- Rate of spread should go perhaps something like:

$$S^*(\sim, p) = \left( \frac{\max(1, U)}{FMI + \sim} \right)^p$$

**2 parameter model.**

where,  $FMI = 10 - 0.25T + 0.25H$

- Or at worst, after applying a dimensional correction...

$$S(r, \sim, p) = r \left( \frac{\max(1, U)}{FMI + \sim} \right)^p$$

**3 parameter model.**

## A SIMPLE INDEX FOR FIRE SPREAD

$$S(r, \sim, p) = r \left( \frac{\max(1, U)}{FMI + \sim} \right)^p, \quad FMI = 10 - 0.25T + 0.25H$$

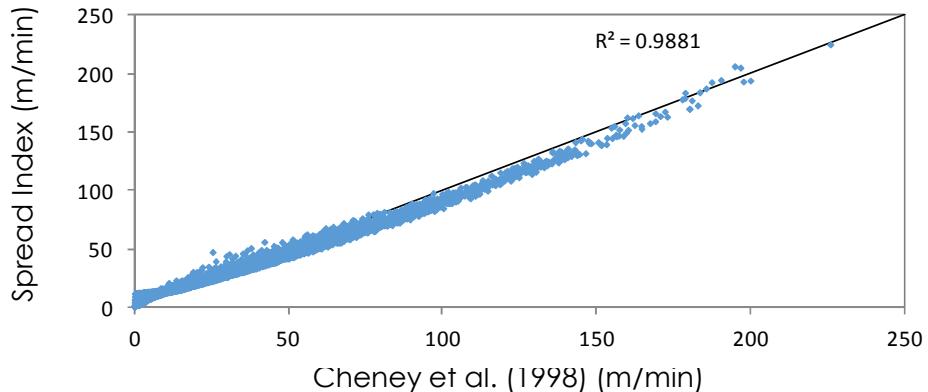
We compare the performance of the simple index with the current operational models for the different fuel types. We assume:

- Fuel factors are constant – so we are only considering the meteorological model components;
- The parameter  $r$  is defined so that the mean values of the spread index and the predictions of the operational models agree.

# **MODEL COMPARISON RESULTS**

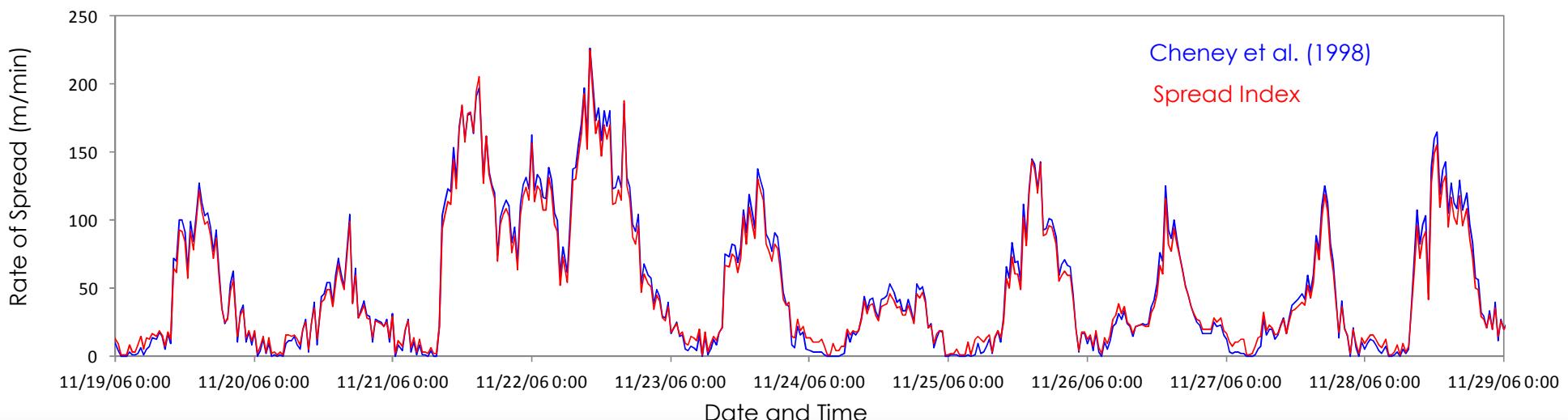
Using approximately 5,000 data points from Canberra airport  
automatic weather station Nov-Mar, 2006.

# GRASSLAND



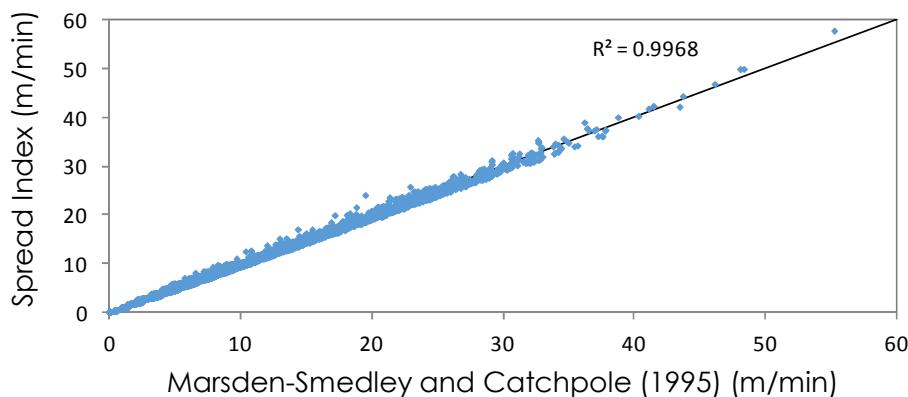
$$S(r, \sim, p) = r \left( \frac{\max(1, U)}{FMI + \sim} \right)^p,$$

| $r$ (m/min) | $\sim$ | $p$ |
|-------------|--------|-----|
| 46.1        | 5.2    | 1.0 |



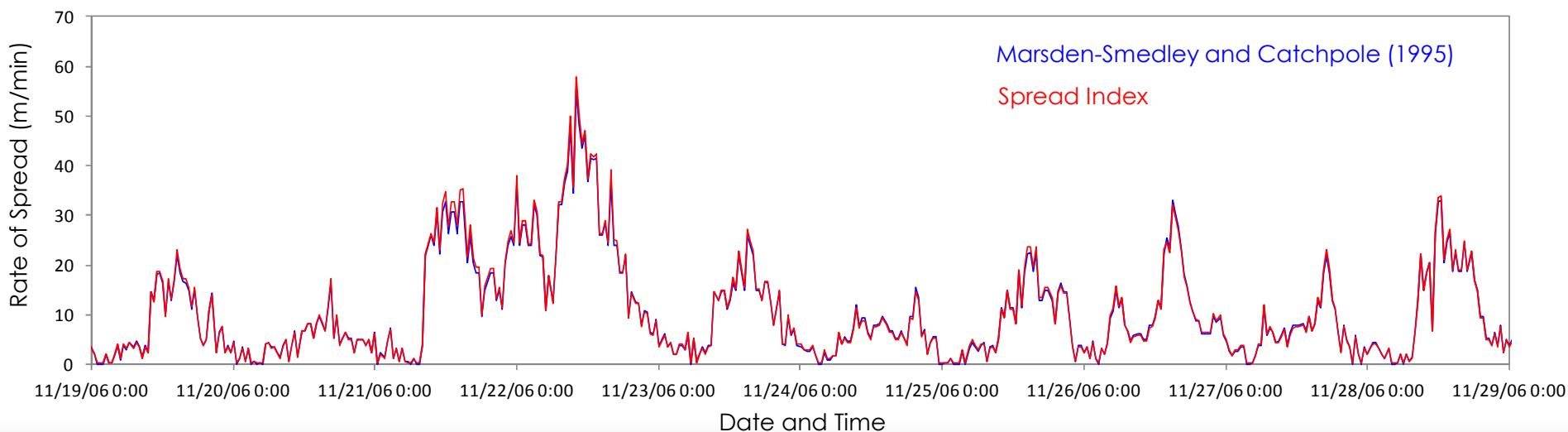
$C = 100\%$

# BUTTONGRASS MOORLAND



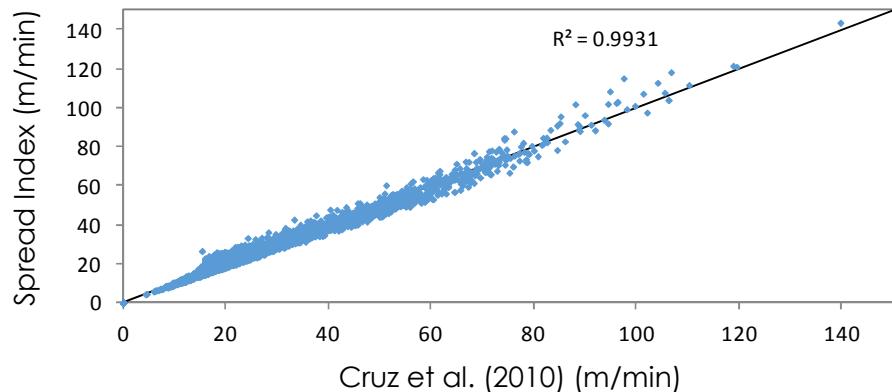
$$S(r, \sim, p) = r \left( \frac{\max(1, U)}{FMI + \sim} \right)^p,$$

| r (m/min) | ~    | p   |
|-----------|------|-----|
| 104.5     | 80.0 | 1.3 |



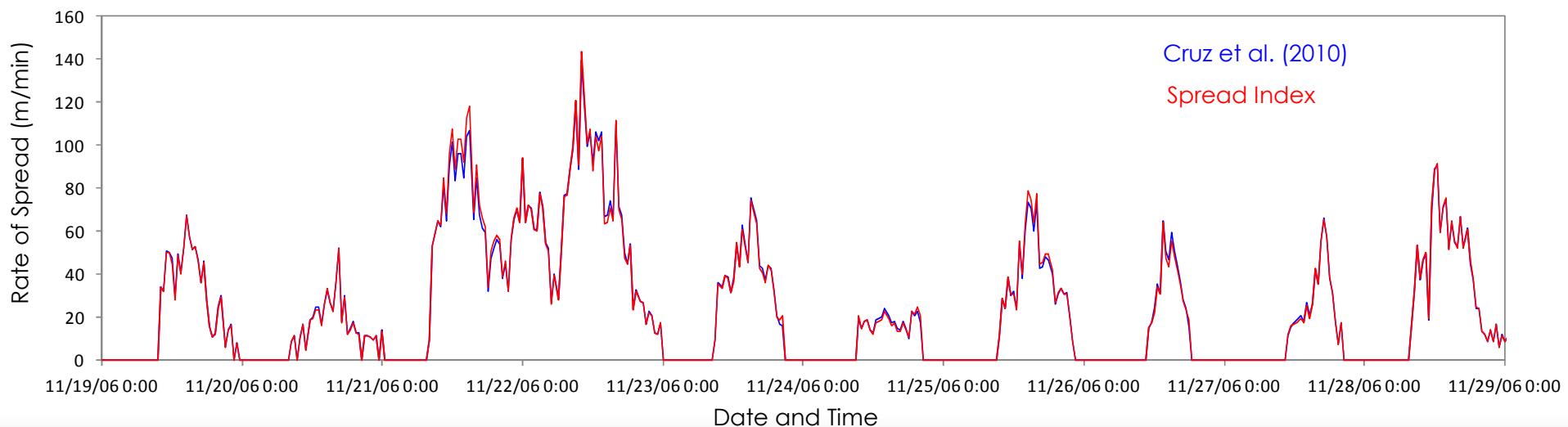
AGE = 16 years

# S.A. HEATH



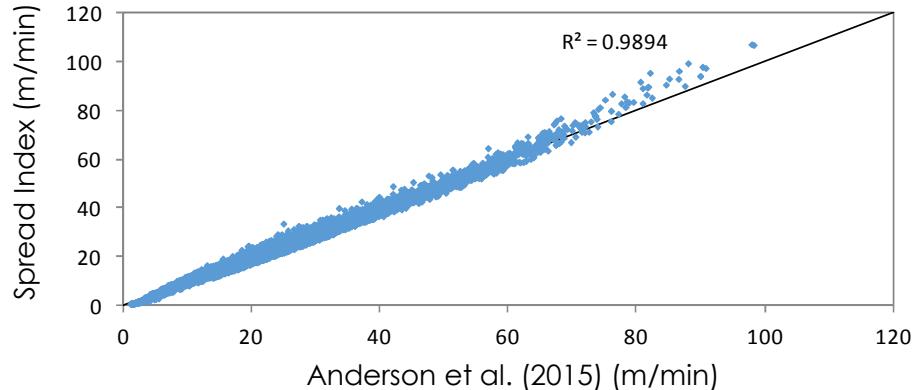
$$S(r, \sim, p) = r \left( \frac{\max(1, U)}{FMI + \sim} \right)^p,$$

| $r$ (m/min) | $\sim$ | $p$ |
|-------------|--------|-----|
| 27.9        | 8.0    | 1.2 |



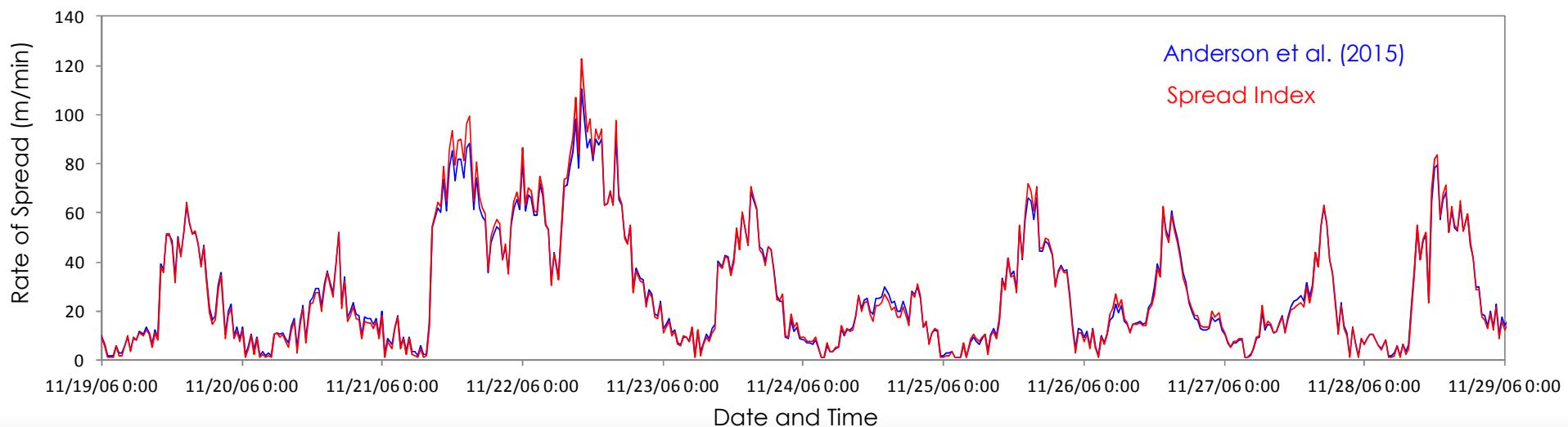
$$FHS_{el} = PCS_{ns} = 3$$

# TEMPERATE SHRUBLAND



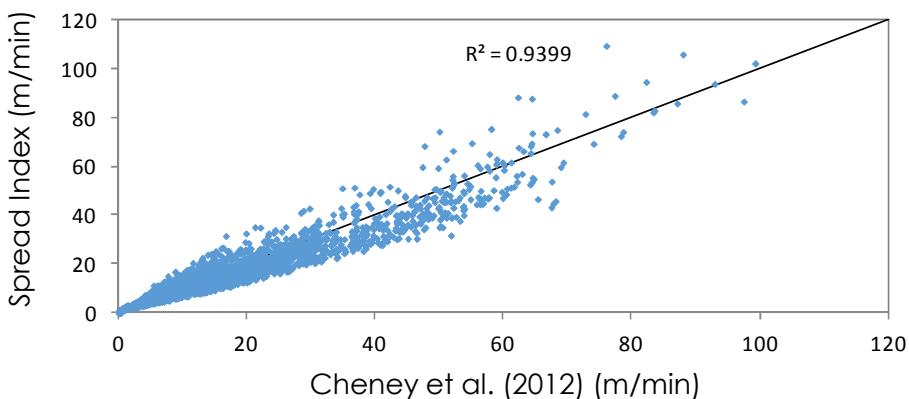
$$S(r, \sim, p) = r \left( \frac{\max(1, U)}{FMI + \sim} \right)^p,$$

| $r$ (m/min) | $\sim$ | $p$ |
|-------------|--------|-----|
| 37.9        | 11.0   | 1.0 |



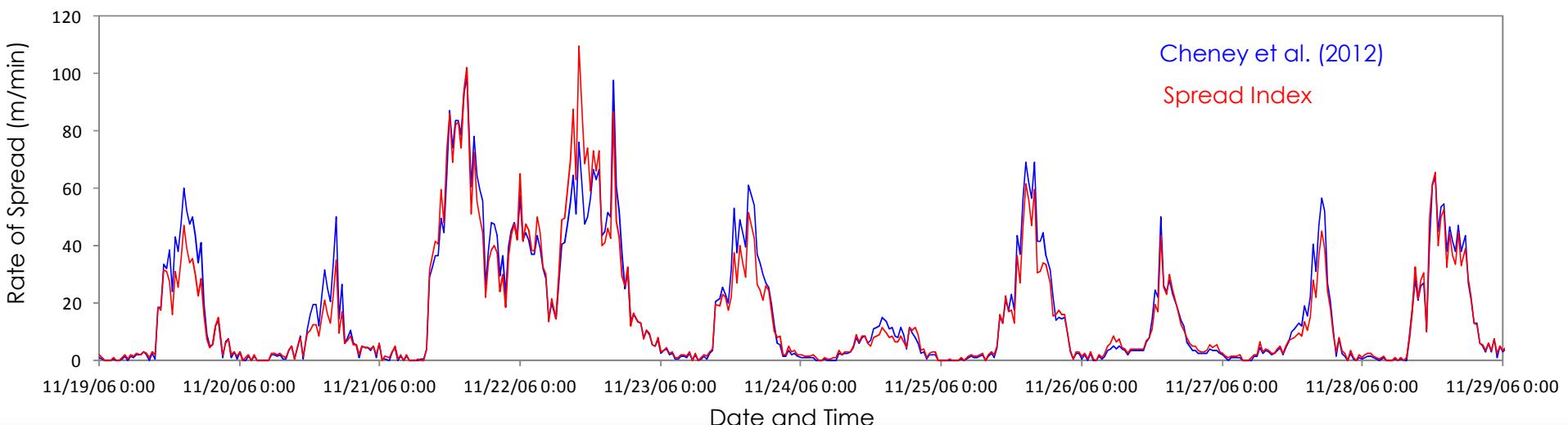
$h = 2 \text{ m}$

# DRY EUCALYPT FOREST



$$S(r, \sim, p) = r \left( \frac{\max(1, U)}{FMI + \sim} \right)^p,$$

| $r$ (m/min) | $\sim$ | $p$ |
|-------------|--------|-----|
| 10.2        | 4.0    | 1.4 |



$$FHS_s = FHS_{ns} = 2, \quad h_{ns} = 100 \text{ cm}$$

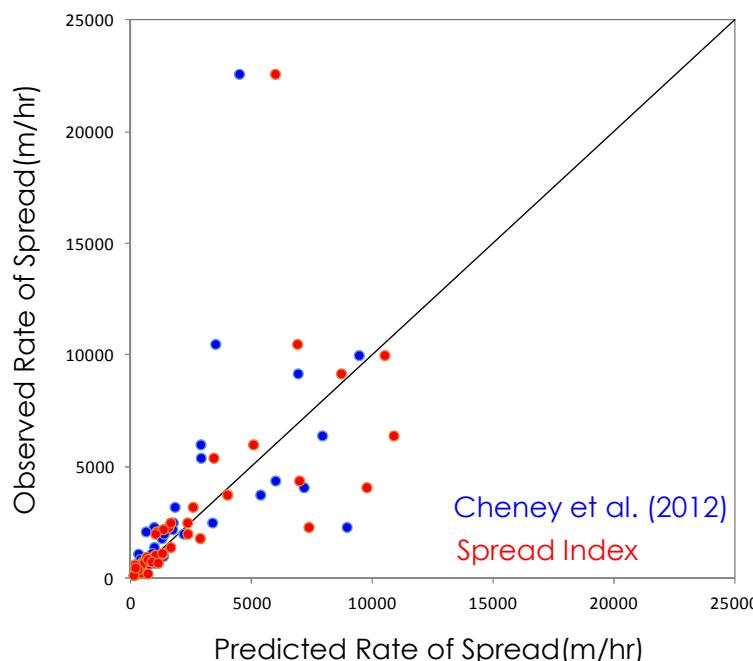
## SUMMARY OF MODEL COMPARISON RESULTS...

| Vegetation type*     | r (m/min) | ~    | p   | R <sup>2</sup> |
|----------------------|-----------|------|-----|----------------|
| Grasslands           | 46.1      | 5.2  | 1.0 | 0.988          |
| Buttongrass moorland | 104.5     | 80.0 | 1.3 | 0.997          |
| Mallee-Heath         | 27.9      | 8.0  | 1.2 | 0.993          |
| Temperate shrubland  | 37.9      | 11.0 | 1.0 | 0.989          |
| Dry eucalypt forest  | 10.2      | 4.0  | 1.4 | 0.940          |

\* For the particular fuel parameters used.

## SOME MORE ON THE DRY EUCALYPT FOREST MODEL...

- Cheney et al. (2012) compare the predictions of the dry eucalypt fire spread model with observations of wildfire rate of spread.
- So we can do the same with the spread index...!



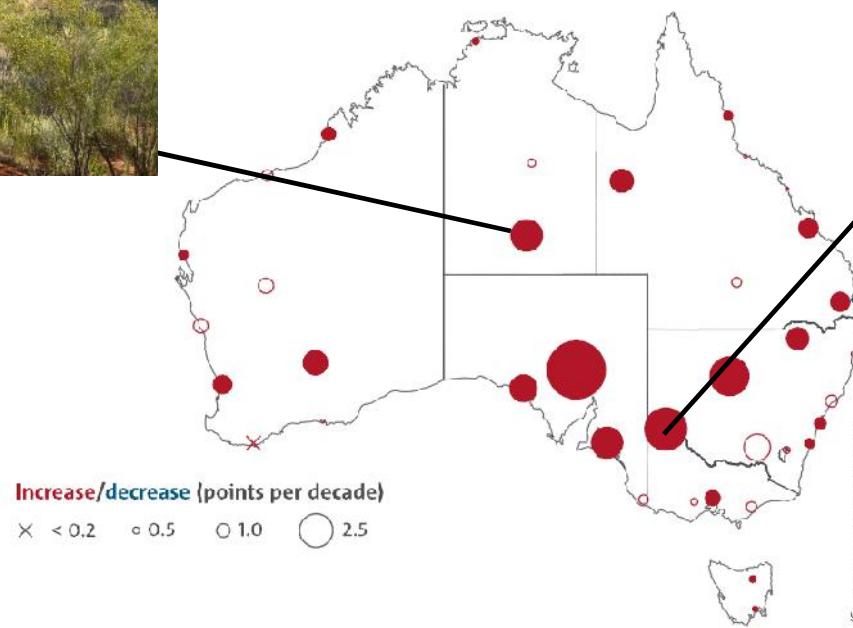
| Model                | MAE | MBE  |
|----------------------|-----|------|
| Cheney et al. (2012) | 51% | -24% |
| Spread Index*        | 44% | -8%  |

\* Note that the spread index doesn't incorporate any info on fuel structure, whereas the model of Cheney et al. (2012) does!

# IMPLICATIONS FOR NATIONAL FIRE DANGER RATING...



Change in FFDI  
1974-2015



## CONCLUSIONS

- The results confirm, once and for all, that current operational fire spread models are needlessly complicated...!
- A single, universal functional form can be used to predict rate of spread across all of the fuel types considered, without any appreciable loss in model performance...!
- The universal model is far more parsimonious, with half to a quarter of the model parameters of accepted fire spread models...!
- The universal model is also far more conceptually simple: rate of spread is essentially ‘wind speed divided by fuel moisture content’...!
- Spinifex still presents a bit of a challenge... but fits with the general philosophy...!